

# **Multi-Function PLL System**

# **GENERAL DESCRIPTION**

The XR-S200 integrated circuit is a highly versatile, multipurpose circuit that contains all of the essential functions of most communication system designs on a single monolithic substrate. The function contained in the XR-S200 include: 1. a four quadrant analog multiplier, 2. a high frequency voltage controlled oscillator (VCO) and 3. a high performance operational amplifier.

The three functions can be used independently, or directly interconnected in any order to perform a large number of complex circuit functions, from phase-locked loops to the generation of complex waveforms. The XR-S200 can accommodate both analog and digital signals, over a frequency range of 0.1 Hz to 30 MHz, and operate with a wide choice of power supplies extending from  $\pm 3$  volts to  $\pm 30$  volts.

# FEATURES

Wide VCO Frequency Range0.1 Hz to 30 MHzWide Supply Voltage Range± 3V to ± 30 VUncommitted Inputs and Outputs for MaximumFlexibilityLarge Input Dynamic Range

# APPLICATIONS

Phase-locked loops FM demodulation Narrow and wideband FM Commercial FM-IF TV sound and SCA detection FSK detection (MODEM) PSK demodulation Signal conditioning Tracking filters Frequency synthesis Telemetry coding/decoding AM detection Quadrature detectors Synchronous detectors Linear sweep & AM generation Crystal controlled Suppressed carrier Double sideband Tone generation/detection Waveform generation Single/square/triangle/sawtooth Analog multiplication

# FUNCTIONAL BLOCK DIAGRAM



## ABSOLUTE MAXIMUM RATINGS

Power Supply	30 Volts
Power Dissipation	900 mW
Derate above +25°C	5 mW/°C
Temperature	
Operating	-55°C to +125°C
Storage	-65°C to +150°C
Input Signal Level, V <sub>S</sub>	6 V,p-p

### **ORDERING INFORMATION**

Part Number	Package	Operating Temperature
XR-S200	Ceramic	0°C to +70°C

# **ELECTRICAL SPECIFICATIONS** (T = $25^{\circ}$ C, V<sub>SUPPLY</sub> = $\pm 10$ V)

	LIMITS							
PARAMETERS	MIN	ТҮР	MAX	UNITS	CONDITIONS			
<b>MULTIPLIER SECTION:</b> See Figure 2, $R_X = R_y = 15k$ , Pins 1, 2, 6, 23, 24 Grounded.								
Output Offset Voltage Input Bias Current Input Offset Current		±40 5 0.1	± 120 15 1.0	mV μA μA	$V_X = V_y = 0$ , $V_{10} =  V_3 - V_4 $ Measured at pins 5 and 7 Measured at pins 5 and 7			
(Output error, % of full scale) Scale Factor, K <sub>M</sub> Input Resistance 3 dB Bandwidth Phase detection B.W. Differential Output Swing Output Impedance	0.3 3 50 ±4	1.0 1.5 0.1 1.0 6 100 ±6		% - MΩ MHz MHz V p-p	$\begin{array}{l} -5 < V_X < \pm 5, V_y = \pm 5V \\ -5 < V_V < \pm 5, V_X = \pm 5V \\ K_M = 25/R_XR_y \text{ (Adjustable)} \\ f = 20 \text{ Hz}, \text{ Measured at pins 5 and 7} \\ C_L \leq 5 \text{ pF} \\ R_X = R_y = 0 \\ \text{Measured across pins 3 and 4} \end{array}$			
Single Ended		6		kΩ kΩ	Measured at pins 3 and 4			
<b>OPERATIONAL AMPLIFIER SECTION:</b> See Figure 10 and 11, $R_L = 20k$ , $C_L = 550 pF$ .								
Input Bias Current Input Offset Current Input Offset Voltage Differential Input Impedance		0.08 0.02 1.0	0.5 0.2 6.0	μA μA mVdc	Open loop f - 20 Hz			
Resistance Capacitance Common Mode Range Common Mode Rejection Open Loop Voltage Gain	0.4 70 66	2.0 1.0 ±8 90 80		MΩ pF V dB dB	f = 20 Hz			
Output Impedance Output Voltage Swing Power Supply Sensitivity Slew Rate	±7	2 ±9 30 2.5		kΩ V μV/V V/μsec	$\begin{array}{l} R_{L} \geq 20 \; k\Omega \\ R_{S} \leq 10 \; k\Omega \\ A_{V} = 1, \; C_{L} = \; 10 \; pF \end{array}$			
VC0 SECTION: See Figure 11,	$R_L = 10$	0k, f <sub>0</sub> = 1	MHz.					
Upper Frequency Limit Sweep Range	15 8:1	30 10:1		MHz –	$C_0 = 10 \text{ pF}$ f <sub>0</sub> = 10 kHz, See Figure 14 Digital Controls Off			
(distortion for $\Delta f/f = 10\%$ )		.2	1.0	%	Digital Controls Off			
Frequency Stability Power Supply Temperature Analog Input Impedance Resistance Capacitance Output Amplitude Output Rise Time	0.1	0.08 300 0.5 1.5 3 15	0.5 650	%/V ppm/°C MΩ pF V p-p ns	$V_{CC} > 8V$ , $f_0 = 1 \text{ MHz}$ Sweep Input Open Measured at pins 23 and 24 Squarewave $C_L = 10 \text{ pF, } R_L = 5 \text{ k}\Omega$			
Fall Time Input Common Mode Range	+6 -4	20 + 8 - 6		ns Vdc Vdc				

CAUTION: When using only some of the blocks within the XR-S200, the input terminals to the unused section must be grounded (for split-supply operation); or connected to an ac ground biased at V<sup>+</sup>/2 (for single supply operation).

# XR-S200 XR-S200 ANALOG MULTIPLIER SECTION

The analog multiplier in the XR-S200 (Figure 2) provides linear four-quadrant multiplication over a broad range of input signal levels. It also serves as a balanced modulator, phase comparator, or synchronous detector. Gain is externally adjustable. Nonlinearity is less than 2% of full scale output.

# TYPICAL APPLICATIONS OF MULTIPLIER SECTION

- · Analog multiplication/division
- Phase detection
- Balanced modulation/demodulation
- Electronic gain control
- Synchronous detection
- Frequency doubling

# ANALOG MULTIPLICATION

The XR-S200 multiplier section can be combined with the amplifier section to perform analog multiplication without the need for dc level shifting between input and output. The amplifier functions as an operational amplifier with a single-ended output at ground level when connected as shown in Figure 3.





# PHASE COMPARATOR

For phase comparison, a low-level reference signal is normally applied to one input and a high-level reference or carrier signal to the other input, as in Figure 4. The signal may be applied to either the X or Y input, since the response is symmetrical.

If the two inputs,  $V_{R}(t)$  and  $V_{S}(t)$  are at the same frequency, then the dc voltage at the output of the phase comparator can be related to the phase angle  $\phi$  between the two signals as

$$V_{\phi} = K_{\phi} \cos \phi$$

where  $K_{\phi}$  is the conversion gain in volts per radian (Figure 5). For phase comparator applications, one input is







Figure 4. XR-S200 Multiplier Section as a Phase Comparator

normally a high level reference signal and the other input a low level information signal. Since the XR-S200 multiplier section offers symmetrical response with respect to the X and Y inputs, either input can be used as the carrier or signal input. For low input levels, the conversion gain is proportional to the input signal amplitude. For high level inputs, (V\_S > 40 mV, rms) K\_{\phi} is constant and approximately equal to 2V/rad.

# SUPPRESSED-CARRIER AM

The multiplier generates suppressed-carrier AM signals when connected as in Figure 6. Again, the symmetrical response allows the X or Y inputs to be used interchangeably as the carrier or modulation inputs. The X and Y offset adjustments optimize carrier suppression. Gain control resistors R<sub>X</sub> and R<sub>Y</sub> typically range from 1 K $\Omega$  to 10 K $\Omega$ , depending on input signal amplitudes. The values shown give approximately 60 dB carrier suppression at 500 kHz and 40 dB at 10 MHz.

## DOUBLE-SIDEBAND AM GENERATION

The connection for double-sideband AM generation is shown in Figure 7. The dc offset adjustment on the modulation input terminal sets the carrier output level, while the dc offset of the carrier input governs symmetry of the output waveform. The modulation input can also be used as a linear gain control (AGC), to control amplification with respect to the carrier input signals.









#### FREQUENCY DOUBLING

Figure 8 shows how to double a sinusoidal input signal of frequency  $f_S$  to produce a low-distortion sinewave output of  $2f_S$ . Total harmonic distortion is less than 0.6% with an input of 4V, p-p, at 10 kHz and an output of 1V, p-p, at 20 kHz. The multiplier's X and Y offsets are nulled as shown to minimize the output's harmonic content.

### SYNCHRONOUS AM DETECTION

A typical synchronous AM detector is shown in Figure 9. The signal is applied to the multiplier common input and the X and Y inputs are grounded. Since the Y input



Figure 7. Double Sideband Amplitude Modulation Using XR-S200 Multiplier Section



Figure 7-1. AM Modulation, 95% AM,  $f_{C}$  = 50 kHz,  $f_{M}$  = 1 kHz



Figure 8. Multiplier Section as Frequency Doubler



operates at maximum gain with  $R_Y = 0$ , the detector gain and demodulated output linearity are determined by  $R_X$ . An  $R_X$  range of 1 K $\Omega$  to 10 K $\Omega$  is recommended for carrier amplitudes of 100 mV, p-p; or greater. The multiplier output can be low-pass filtered to obtain the demodulated output. Figure 9-1 shows the carrier and modulated waveforms for a 30% modulated input signal with a 10 MHz carrier and 1 kHz modulation.



Figure 9. Synchronous AM Detector



Figure 9-1. Synchronous AM Demodulation

# **XR-S200 AMPLIFIER SECTION**

This multi-purpose function (Figure 10) can be used as a general-purpose operational amplifier, high-speed comparator, or sense amplifier. It features an input impedance of 2 megohms, high voltage gain, and a slew rate of 2.5V/microsecond. The frequency response curves for the amplifier section are also shown in Figure 10.



Figure 10. Amplifier Section Frequency Response

# **XR-S200 OSCILLATOR SECTION**

The voltage-controlled oscillator section, (Figure 11) is an exceptionally versatile design capable of operating from a fraction of a cycle to in excess of 40 MHz. Frequencies can be selected and controlled by three methods, and used in various combinations for different applications:

- 1. External timing capacitor  $C_0$  tunes the VCO to a center frequency between 0.1 Hz and 40 MHz. The freerunning frequency is inversely proportional to  $C_0$ . (see Figure 12)
- Two digital control inputs allow four discrete frequencies to be selected at any center frequency. The digital inputs convert the logic signal voltages to internal control currents. (see Figure 13)
- 3. A sweep voltage, applied through a limiting resistor R<sub>S</sub> is used for frequency sweeping, on-off keying, and synchronization of the VCO to a sync pulse. (see Figure 14)

The voltage-to-frequency conversion of the VCO section is highly linear. In addition, the conversion gain can be controlled through the analog control input. Gain is inversely proportional to  $R_0$ . When the digital controls are also used, gain decreases as the frequency is stepped up.

The VCO interfaces easily with ECL or TTL logic. It can be converted to a highly stable crystal-controlled oscillator by simply substituting a crystal in place of the timing capacitor,  $C_0$ .

Typical performance characteristics of the VCO section are shown in Figures 12, 13, and 14.



Figure 11. XR-S200 Oscillator Section



Figure 12. VCO Frequency as a Function of Timing Capacitor, C<sub>0</sub>



Figure 13. VCO Digital Tuning Characteristics

# **XR-S200** EXPLANATION OF VCO DIGITAL CONTROLS

The VCO frequency is proportional to the total charging current,  $I_T$ , applied to the timing capacitor. As shown in Figure 15,  $I_T$  is comprised of three separate components:  $I_0$ ,  $I_1$ , and  $I_2$ , which are contributed by transistors  $T_0$ ,  $T_1$ , and  $T_2$ , respectively. With pins 15 and 16 open circuited, these currents are interrelated as

$$I_0 = I_1 = 2I_2$$

Currents I<sub>1</sub>and I<sub>2</sub> can be externally controlled through pins 16 and 15 respectively. By increasing the dc level at either of these pins, T<sub>1</sub> or T<sub>2</sub> can be turned "off" and I<sub>1</sub> or I<sub>2</sub> can be reduced to zero. With reference to Figure 15, this can be done by applying a 3 volt logic pulse to these pins, through disconnect diodes D<sub>1</sub> and D<sub>2</sub>. In this manner, the VCO frequency can be stepped in four discrete intervals, over a frequency range of 2.5:1, as shown in Figure 13.



8

Figure 14. Voltage Sweep Characteristics



Figure 15. Explanation of VCO Digital Controls

# XR-S200 TYPICAL APPLICATIONS OF VCO SECTION

- Voltage/frequency conversion
- Phase-locked loops
- · Frequency synthesis
- Signal conditioning
- Carrier generation
- Synchronization
- · Sweep and FM generator
- Crystal oscillator
- Waveform generator
- Keyed oscillator

# APPLICATIONS OF THE XR-S200 SYSTEM

### PHASE-LOCKED LOOP

A self-contained phase-locked loop is formed by connecting the XR-S200 as outlined in Figure 16.

In most PLL applications, the amplifier is available for functions useful outside the loop, since the phase comparator (multiplier section) and VCO provide sufficient conversion gain. In this case, the amplifier gain does not enter the PLL gain expression. Assuming unity dc gain for the filter, the PLL loop gain is  $K_T = K_{\phi} K_0$  where  $K_{\phi}$  and  $K_0$  are the multiplier and VCO conversion gains, respectively.



Figure 16. XR-S200 as a Phase-Locked Loop



Figure 17. Circuit Connection for FM Detection

## FREQUENCY-SELECTIVE FM DEMODULATION

For FM demodulation, the PLL connection is used (Figure 17.) The multiplier, with its gain terminals shorted, serves as the phase detector, and the VCO and filter govern the operating frequencies.

The gain block is used as an audio preamplifier to set the demodulated output signal level. Volume is controlled by the variable feedback resistor R<sub>7</sub>. If R<sub>6</sub> equals R<sub>7</sub>, the dc output level will be very close to ground, for circuit operation with split power supplies. C<sub>3</sub> is the amplifier's compensation capacitor. R<sub>8</sub> and C<sub>2</sub> set the output de-emphasis time constant T<sub>D</sub>, which is normally 75  $\mu$ sec. for commercial FM applications (f<sub>0</sub> = 10.7 MHz).

#### **FSK DETECTION**

FSK signals are detected and demodulated with the PLL connection, as well. It is shown in Figure 18 as a monolithic MODEM suitable for Bell 103 or 202 type data sets operating at data rates to 1800 baud. An input frequency shift corresponding to a data bit causes the multiplier's dc voltage output to reverse polarity. The dc level is changed to a binary output pulse by the gain block, connected as a voltage comparator.





### FREQUENCY SYNTHESIZER

Frequency synthesis is performed in Figure 19 by a phase-locked loop closed with a programmable counter or digital divide-by-N circuit inserted into the feedback loop. The VCO frequency is divided by N, so that when the circuit locks to an input signal at frequency  $f_S$ , the

oscillator output is  $Nf_{S}$ . A large number of discrete frequencies can be synthesized from a given reference frequency by changing N.



### Figure 19. Frequency Synthesizer

### TRACKING FILTER AND WIDEBAND DISCRIMINATOR

In tracking filter applications, the XR-S200 again forms a PLL system (Figure 20). When the PLL locks on an input signal, it functions as a "frequency-filter" and produces a filtered version of the input signal frequency at the VCO output. Since it can track the input over a broad range of frequencies around the VCO freerunning frequency, it is also called a "tracking filter". The system can track input signals over a 3:1 frequency range.

## WAVEFORM GENERATOR

The XR-S200 can also be interconnected to form a versatile waveform generator. The typical circuit shown in Figure 21 generates the basic periodic square (or sawtooth) waveform. The multiplier section, connected as a linear differential amplifier, convert the differential sawtooth waveform input into a triangle wave output at pins



Figure 20. Recommended Circuit Connection for Tracking Filter Application ( $f_0 = 1 \text{ MHz}$ )



Figure 21. Waveform Generator Typical Circuit Connection Diagram



Figure 21-1. Basic Waveforms Available from XR-S200

3 and 4. The waveform adjustment pot across pins 8 and 9 can be used to round the peaks of the triangle waveform and convert it to a low distortion sinewave (THD<2%). Terminals 3 and 4 can be used either differentially or single endedly to provide both in-phase and out-of-phase output waveforms.

The output frequency can be swept or frequency modulated by applying the proper analog control input to the circuit. For linear FM modulation with relatively small frequency deviation ( $\Delta f/f < 10\%$ ) the modulation input can be applied across terminals 23 and 24. For large deviation sweep inputs, a negative going sweep voltage, V<sub>S</sub>, can be applied to pin 18.

This allows the frequency to be voltage-tuned over approximately a 10:1 range in frequency. The digital control inputs (15 and 16) can be used for frequency-shift-keying (FSK) applications. They can be disabled by connecting them to ground through a current-limiting resistor.



Figure 22. Circuit Connection for AM/FM or Crystal-Controlled AM Generator Application



Figure 22-1. Double Sideband AM Output Waveform  $f_{carrier} = 3.688 \text{ MHz} f_{mod} = 1 \text{ kHz}$  (90% modulation)

# AM & FM SIGNAL GENERATION

The oscillator and multiplier sections can be interconnected as a general purpose radio-frequency signal generator with AM, FM and sweep capability as shown in Figure 22.

The oscillator section can be used as a voltage-tuned, variable frequency oscillator, or as a highly stable carrier or reference generator by connecting a reference crystal across terminals 19 and 20. In this case, a small capacitor (typically 10 to 100 pF) fine tunes the crystal frequency. The multiplier section introduces the amplitude modulation on the carrier signal generated by the VCO. The balanced nature of the multiplier allows suppressed carrier as well as double sideband modulation (Figures 22-1 and 22-2). Typical carrier suppression is in excess of 40 dB for frequencies up to 10 MHz.

If a timing capacitor is used instead of a crystal, the oscillator section can provide highly linear FM or frequency sweep. The digital control terminals of the oscillator are used for frequency-shift-keying.



Figure 22-2. Suppressed Carrier AM Output Waveform  $f_{carrier} = 3.688 \text{ MHz } f_{mod} = 1 \text{ kHz}$ 



EQUIVALENT SCHEMATIC DIAGRAM