CAT7117 Dual Channel 800mA High Efficiency Step-Down DC/DC Converter

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General Description

The CAT7117 is a high efficiency step-down DC/DC converter using a constant frequency, current mode architecture. The device integrates a main switch and a synchronous rectifier for high efficiency without an external schottky diode. Supply current during operation is only 300µA and drops to \leq 1µA in shutdown. The CAT7117 can supply 800mA of load current from 2.5V to 5.5V input voltage. The output voltage can be regulated as low as 0.6V.

Switching frequency is internally set at 1.8MHz, allowing the use of small surface mount inductors and capacitor. It can also run 100% duty cycle for low dropout applications.

Application

- Cellular Telephones
- PDAs and Smart Phones
- MP3 Players
- Microprocessors and DSP Core Supplies
- Wireless and DSL Card
- Digital Still Cameras
- Slim-Type DVD
- Portable Instruments

Pin Configuration

TOP VIEW



Typical Application



Features

- High Efficiency up to 95%
- Low Quiescent Current < 300uA (active mode)
- ♦ 2.5V to 5.5V Input Voltage Range
- 800mA Output Current on each Channel
- Fix Frequency Operation
- ◆ Full Duty ratio, 0 100% in Dropout
- 0.6V Reference Allows Low Output Voltages
- Current Mode Operation
- Internal soft-start
- Over-temperature Protected
- ♦ < 0.1µA Shutdown Current</p>
- DFN3x3 small Package
- RoHS Compliant (100% Green available)

Ordering Information

Part Number	Package	Ship		
CAT7117CE	DFN10 3x3	2500/ Tape & Reel		

Efficiency Table

Efficiency VS Output Current at VIN=5V



Pin Description

Pin	Symbol	Description
		Channel1 Regulator enable control input Pin. Drive EN1 above 1.5V to turn on
1	EN1	Channel1.
		Drive EN1 below 0.3V to turn it off (shutdown current < 0.1uA).
2	FB1	Channel1 Voltage feedback Pin.
3	VIN2	Channel2 Main supply Pin.
4	GND2	Channel2 Ground Pin.
5	SW2	Channel2 Power switch output
		Channel2 Regulator enable control input Pin. Drive EN2 above 1.5V to turn on
6	EN2	Channel2.
		Drive EN2 below 0.3V to turn it off (shutdown current < 0.1uA).
7	FB2	Channel2 Voltage feedback Pin.
8	VIN1	Channel1 Main supply Pin.
9	GND1	Ground Pin.
10	SW1	Channel1 Power switch output

Function Block Diagram



Absolute Maximum Ratings

Package Thermal Characteristics

Thermal Resistar	nce	θJA	θJC	
DFN10 3mx3m		. 50	10	°C/W

*note1: The IC has a protection circuit against static electricity. Do not apply high static electricity or high voltage that exceeds the performance of the protection circuit to the IC.

*note2: Fully production test at +25°C. Specificati ons over the temperature range are guaranteed by design and characterization.

Electrical Characteristic

(Recommended Operating Conditions, Unless Otherwise Noted; V_{IN} = 3.6V; Temperature = 0 - 70 °C (typical = 25 °C))

Parameter	Symbol	Test Conditions	Min	Тур.	Max	Unit
Supply Voltage	V _{IN}		2.5		5.5	V
Feedback Current	I _{VFB}		-30	0.5	30	nA
Regulated Feedback Voltage	V_{FB}	T _A = 25°C -40°C ≦T _A ≦85°C	0.588 0.582	0.6 0.6	0.612 0.618	V
Reference Voltage Line Regulation	$ riangle V_{FB}$	$V_{IN} = 2.5V$ to 5.5V		0.04	0.4	%V
Output Voltage Line Regulation	$ riangle V_{OUT}$	$V_{IN} = 2.5V$ to 5.5V		0.04	0.4	%V
Output Voltage Load Regulation	V_{LOADRGE}			0.5		%
Shutdown Current	I _S	$V_{EN} = 0V, V_{IN} = 5.5V$		0.01	1	μA
Quiescent Current	Ι _Q	$V_{EN} = V_{IN}, V_{FB} = 0.65V,$ No switching		300		μA
SW Leakage Current	I _{LEAK}	$V_{EN} = 0V, V_{IN} = 5.5V$ $V_{SW} = 0V \text{ or } 5.5V$	-1		1	μA
PMOSFET On Resistance	R _{DSONP}	I _{SW} = 100mA		0.35		Ω
NMOSFET On Resistance	R _{DSONN}	I _{SW} = -100mA		0.24		Ω
PMOSFET Current Limit	I _{PCL}	Duty Cycle = 100% Current Pulse Width < 1ms	0.9	1.2	1.4	А
Oscillator Frequency	Fosc		1.2	1.6	2.0	MHz
Thermal Shutdown Threshold	Τs			145		°C
EN high level input voltage	V _{EN}	- 40°C \leq T _A \leq +85°C	0.9			V
EN low level input voltage	V _{EN}	-40° C $\leq T_{A} \leq +85^{\circ}$ C			0.3	V
EN Input Current	I _{EN}	$V_{EN} = 0V \text{ to } V_{IN}$	-1		1	μA

*note: Fully production test at +25°C. Specifications over the temperature range are guaranteed by design and characterization.

Function Description

The CAT7117 is a constant frequency current mode PWM step-down converter. The CAT7117 is optimized for low voltage, Li-lon battery powered applications where high efficiency and small size are critical. The CAT7117 uses an external resistor divider to set the output voltage from 0.6V to 5.5V. The device integrates both a main switch and a synchronous rectifier, which provides high efficiency and eliminates an external Schottky diode. The CAT7117 can achieve 100% duty cycle. The duty cycle D of a step-down converter is defined as: D = TON * FOSC * 100% \approx VOUT/VIN * 100% where TON is the main switch on time, and FOSC is the oscillator frequency.

Current Mode PWM Control

Slope compensated current mode PWM control provides stable switching and cycle-by-cycle current limit for superior load and line response and protection of the internal main switch and synchronous rectifier. The CAT7117 switches at a constant frequency (1.8MHz) and regulates the output voltage. During each cycle the PWM comparator modulates the power transferred to the load by changing the inductor peak current based on the feedback error voltage. During normal operation, the main switch is turned on for a certain time to ramp the inductor current at each rising edge of the internal oscillator, and switched off when the peak inductor current is above the error voltage. When the main switch is off, the synchronous rectifier will be turned on immediately and stay on until either the next cycle starts or the inductor current drops to zero. The device skips pulses to improve efficiency at light load.

Internal soft-start

The CAT7117 features an internal soft-start function, which reduces inrush current and overshoot of the output voltage. Soft-start is achieved by ramping up the reference voltage (V_{ref}) which is applied to the input of the error amplifier. The typical soft-start time is about 2 msec and depends on components values on AP circuit.

Dropout Operation

The CAT7117 allows the main switch to remain on for more than one switching cycle and increases the duty cycle while the input voltage is dropping close to the output voltage. When the duty cycle reaches 100%, the main switch is held on continuously to deliver current to the output up to the P MOSFET current limit. The output voltage then is the input voltage minus the voltage drop across the main switch and the inductor.

Short Circuit Protection

The CAT7117 has short circuit protection. When the output is shorted to ground, the oscillator frequency is reduced to prevent the inductor current from increasing beyond the P MOSFET current limit. The P MOSFET current limit is also reduced to lower the short circuit current. The frequency and current limit will return to the normal values once the short circuit condition is removed and the feedback voltage reaches 0.6V.

Maximum Load current

The CAT7117 can operate down to 2.5V input voltage; however the maximum load current decreases at lower input due to large IR drop on the main switch and synchronous rectifier. The slope compensation signal reduces the peak inductor current as a function of the duty cycle to prevent sub-harmonic oscillations at duty cycles greater than 50%. Conversely the current limit increases as the duty cycle decreases match other diagrams in this datasheet.

Input Capacitor Selection

The input capacitor has to sustain the ripple current produced during the on time of the upper MOSFET, so it must have a low ESR to minimize the losses. The RMS value of this ripple is:

$$I_{IN}RMS = I_{OUT} \sqrt{D \times (1-D)}$$

where D is the duty cycle, I_{inRMS} is the input RMS current, and I_{OUT} is the load current. The equation reaches its maximum value with D = 0.5. Losses in the input capacitors can be calculated with the following equation:

$$P_{CIN} = ESR_{CIN} \times I_{IN} RMS^2$$

where P_{CIN} is the power loss in the input capacitors and ESR_{CIN} is the effective series resistance of the input capacitance. Due to large dl/dt through the input capacitors, electrolytic or ceramics should be used. If a tantalum must be used, it must be surge protected. Otherwise, capacitor failure could occur.

Output Inductor Selection

The output inductor is selected to meet the output voltage ripple requirements and affects the load transient response. Higher inductance reduces the inductor's ripple current and induces lower output ripple voltage. The ripple voltage and current are approximated by the following equations:

$$\Delta \mathbf{I} = \frac{\mathbf{V}_{\text{in}} - \mathbf{V}_{\text{out}}}{\mathbf{F}_{\mathbf{S}} \times \mathbf{L}} \bullet \frac{\mathbf{V}_{\text{out}}}{\mathbf{V}_{\text{in}}}$$

$$\Delta \mathbf{V}_{\text{out}} = \Delta \mathbf{I} \times \mathbf{ESR}$$

Although increase the inductance reduce the ripple current and voltage, but the large inductance reduces the regulator's response time to load transient. Increasing the switching frequency (Fs) for a given inductor also reduces the ripple current and voltage but it will increase the switching loss of the power MOS.

To select the inductor value, a guideline is to choose the ripple current (\triangle I) to be approximately \triangle V_{ESR} = change in output voltage due to ESR

(assigned by the designer).

 \triangle IOUT = load transient.

ESR_{CAP} = maximum ESR per capacitor (specified

in manufacturer's data sheet).

ESR_{MAX} = maximum allowable ESR.

High frequency decoupling capacitors should be placed as close to the power pins of the load as physically possible. Consult the capacitors manufacturer to make sure the decoupling requirements. 10%~50% of the maximum output current. Once the inductor value has been chosen, select an inductor that is capable of carrying the required peak current without going into saturation. It is also important to have the inductance tolerance specified to keep the accuracy of the system controlled. Using 20% for the inductance (at room temperature) are reasonable tolerances that most manufacturers can meet. In some types of inductors, especially core that is made of ferrite, the ripple current will increase abruptly when it saturates. This will result in a larger output ripple voltage.

Output Capacitors Selection

An output capacitor is required to filter the output and supply the load transient current. Higher capacitor value and lower ESR reduce the output ripple and the load transient drop. These requirements are met with a mix of capacitors and careful layout.

In typical switching regulator design, the ESR of the output capacitor bank dominates the transient response. The number of output capacitors can be determined by using the following equations:

$$ESR_{MAX} = \frac{\Delta V_{ESR}}{\Delta I_{OUT}}$$

Number Of Capacitors =
$$\frac{ESR_{CAP}}{ESR_{MAX}}$$

Output Voltage

The output voltage is set using the FB pin and a resistor divider connected to the output as shown in next page AP Circuit. The FB pin voltage is 0.6V, so the ratio of the feedback resistors sets the output voltage according to the following equation:

$$V_{FB} = V_{out} \times \frac{R_2}{(R_1 + R_2)}$$

Thus the output voltage is:

$$V_{out} = 0.6 \times \frac{(R_1 + R_2)}{R_2}$$

V _{OUT}	L1/L2	R2/R3	R1/R4	
3.3V	4.7uH	300K Ω	68Κ Ω	
1.8V	4.7uH	1MΩ	500ΚΩ	
1.2V	4.7uH	300K Ω	300K Ω	
1.0V	4.7uH	220ΚΩ	330K Ω	

CAT7117 AP Circuit

C1) R1 Ç2 10nF Vin1, Vin2=2.5V~5.5V Vout1=0.6*(1+R2/R1) R2 Vout2=0.6*(1+R3/R4) C3 <u>\10uF</u> U1 L1 CAT7117 чI EN11 10 EN1 SW1 65 Ċ4 9 FB1 GND1 3.3V 0.1uF Vin13 Vin1 <u>(0.1uF</u> VIN2 IN1 2^{||}4 5 GND2 SW2 ⊢ FB2 C7 6 EN2 EN2 L2 C8 10uF Ξ ~ R3 R4 ,10nF C10 C9 t f EN1 R5 100K R6 100K (<u>C11</u>) Vin1 Vin1 IP1 IP2 G |||ı 00 φ OFF ON ON OFF

1.8V 0

EN2 C12

<u>(0.1uF</u>

llı.

C6

10uF

Package Dimensions

DFN3X3 PACKAGE



COD DOL 6	DIMENSIONS IN MILLIMETERS			
SIMBOLS	MIN NOM		MAX	
А	0.80	0.85	0.90	
A1	0	0.010	0.030	
A3		0.20REF.		
b	0.18	0.23	0.28	
D	2.95	3.00	3.03	
D1		2.20BSC		
Е	2.95	3.00	3.03	
E1		1.60BSC		
e		0.5BSC		
L	0.35	0.40	0.45	
ссс		0.08		
М			0.05	
θ	-12		0	
Burr	0	0.03	0.06	

Classification Reflow Profiles

Reflow Profile	Green Assembly		
Average Ramp-Up Rate (Ts _{max} to Tp)	3℃/second max.		
Preheat			
-Temperature Min(Ts _{min})	150 ℃		
-Temperature Max(Ts _{max})	200 °C		
-Time(ts _{min} to ts ts _{max})	60-180 seconds		
Time maintained above:	217℃		
-Temperature(T _L)	60-150 seconds		
-Time(t _L)			
Peak Temperature(Tp)	260 +0/-5 ℃		
Time within 5 $^\circ\!\!\mathbb{C}$ of actual Peak Temperature(tp)	20-40 seconds		
Ramp-Down Rate	6℃/second max.		
Time 25°C to Peak Temperature	8 minutes max.		

Note: All Temperature refer to topside of the package, measured on the package body surface.



Carrier Tape & Reel Dimensions

Carrier Tape





Cover Tape







note: item: $13^{"}REEL$ ANTI-STATIC $\leq 10^{10} \Omega / \Box$ material: P.S

SPEC	12	16	24	32	44	56	72
DIM A +1.5 -0.5	12.5	16.5	24.5	32.5	44.5	57	73
DIM B ±0.2	2.3	2.3	2.3	2.3	2.3	2.3	2.3
DIM C ±1.5	99	99	99	99	99	99	99

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