

# **AS1310**

# **Ultra Low Quiescent Current, Hysteretic DC-DC Step-Up Converter**

#### **General Description**

The AS1310 is an ultra low quiescent current hysteretic step-up DC-DC converter optimized for light loads (60mA), where it achieves efficiencies of up to 92%.

AS1310 operates from a 0.7V to 3.6V supply and supports output voltages between 1.8V and 3.3V. Besides the available AS1310 standard variants any variant with output voltages in 50mV steps are available.

If the input voltage exceeds the output voltage the device is in a feed-through mode and the input is directly connected to the output voltage.

In light load operation, the device enters a sleep mode when most of the internal operating blocks are turned OFF in order to save power. This mode is active approximately 50µs after a current pulse provided that the output is in regulation.

In order to save power the AS1310 features a shutdown mode, where it draws less than 100nA. During shutdown mode the battery is disconnected from the output.

The AS1310 also offers adjustable low battery detection. If the battery voltage decreases below the threshold defined by two external resistors on pin LBI, the LBO output is pulled to logic

The AS1310 is available in a TDFN (2x2) 8-pin package.

Ordering Information and Content Guide appear at end of datasheet.

#### **Key Benefits & Features**

The benefits and features of AS1310, Ultra Low Quiescent Current, Hysteretic DC-DC Step-Up Converter are listed below:

Figure 1: **Added Value of Using AS1310** 

Benefits	Features
Ideal for single Li-Ion battery powered applications	<ul> <li>Wide Input Voltage Range (0.7V to 3,6V)</li> <li>Feed through mode when V<sub>IN</sub> &gt; V<sub>OUT</sub></li> </ul>
Extended battery life	<ul> <li>High Efficiency up to 92%</li> <li>Low Quiescent Current of typ. 1uA</li> <li>Low Shutdown Current of less than 100nA</li> </ul>
Supports a variety of end applications	<ul> <li>Fixed output voltage range (1.8V to 3.3V)</li> <li>Output Disconnect in shutdown</li> <li>Output current: 60mA @ VIN=0.9V, VOUT=1.8V</li> </ul>

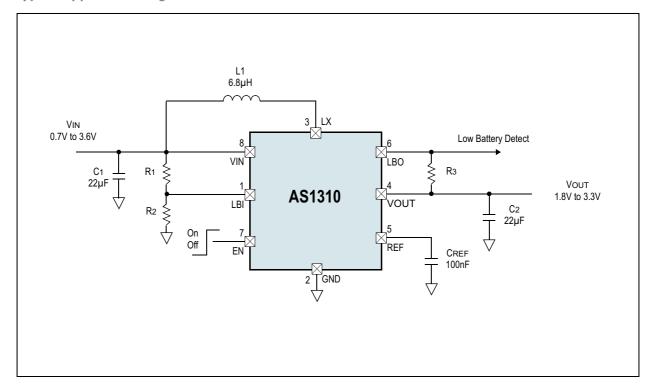


Benefits	Features
Over – temperature protection and shutdown	Integrated temperature monitoring
Early power-fail warning	Adjustable low battery detection
Cost effective, small package	<ul> <li>No external diode or transistor required</li> <li>8-pin TDFN (2mm x 2mm)</li> </ul>

### **Applications**

The AS1310 is an ideal solution for single and dual cell powered devices as blood glucose meters, remote controls, hearing aids, wireless mouse or any light-load application.

Figure 2: Typical Application Diagram



Page 2ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



# **Pin Assignment**

Figure 3: Pin Diagram (Top View)

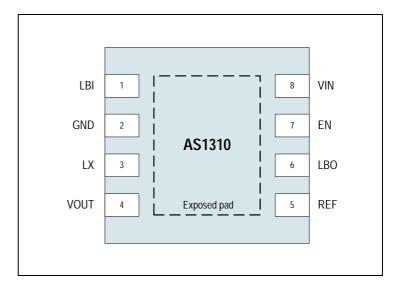


Figure 4: Pin Description

Pin Number	Pin Name	Description
1	LBI	<b>Low Battery Comparator Input</b> . 0.6V Threshold. May not be left floating. If connected to GND, LBO is working as Power Output OK.
2	GND	Ground
3	LX	External Inductor Connector
4	V <sub>OUT</sub>	<b>Output Voltage.</b> Decouple $V_{OUT}$ with a ceramic capacitor as close as possible to $V_{OUT}$ and <b>GND</b> .
5	REF	Reference Pin. Connect a 100nF ceramic capacitor to this pin.
6	LBO	Low Battery Comparator Output. Open-drain output.
7	EN	Enable Pin. Logic controlled shutdown input.  1 = Normal operation;  0 = Shutdown; shutdown current < 100nA.
8	V <sub>IN</sub>	<b>Battery Voltage Input.</b> Decouple $V_{IN}$ with a $22\mu F$ ceramic capacitor as close as possible to $V_{IN}$ and GND.
9	NC	<b>Exposed Pad.</b> This pad is not connected internally. Can be left floating or connect to <b>GND</b> to achieve an optimal thermal performance.

ams Datasheet Page 3
[v1-11] 2015-Jan-28
Document Feedback



### **Absolute Maximum Ratings**

Stresses beyond those listed in Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in Electrical Characteristics is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

Figure 5:
Absolute Maximum Ratings

Parameter	Min	Max	Units	Comments
		Electrical Paran	neters	
V <sub>IN</sub> , V <sub>OUT</sub> , EN, LBI, LBO to GND	-0.3	+5	V	
LX, REF to GND	-0.3	V <sub>OUT</sub> + 0.3	V	
Input Current (latch-up immunity)	-100	100	mA	Norm: JEDEC 78
	E	lectrostatic Dis	charge	
Electrostatic Discharge HBM		±2	kV	Norm: MIL 883 E method 3015
Tel	mperatur	e Ranges and S	torage Con	ditions
Thermal Resistance $\theta_{JA}$		58	°C/W	
Junction Temperature		+125	°C	
Storage Temperature Range	-55	+125	°C	
Package Body Temperature		+260	°C	The reflow peak soldering temperature (body temperature) specified is in accordance with IPC/JEDEC J-STD-020"Moisture/Reflow Sensitivity Classification for Non-Hermetic Solid State Surface Mount Devices".  The lead finish for Pb-free leaded packages is matte tin (100% Sn).
Humidity non-condensing	5	85	%	
Moisture Sensitive Level		1		Represents a maximum floor life time of unlimited

Page 4

Document Feedback

[v1-11] 2015-Jan-28



#### **Electrical Characteristics**

All limits are guaranteed. The parameters with Min and Max values are guaranteed by production tests or SQC (Statistical Quality Control) methods.

 $V_{IN}$  = 1.5V, C1 = C2 = 22 $\mu$ F, C<sub>REF</sub> = 100nF, Typical values are at  $T_{AMB}$  = +25°C (unless otherwise specified). All limits are guaranteed. The parameters with min and max values are guaranteed with production tests or SQC (Statistical Quality Control) methods.

Figure 6: Electrical Characteristics

Symbol	Parameter	Conditions	Min	Тур	Max	Units
T <sub>AMB</sub>	Operating Temperature Range		-40		+85	°C
		Input				
V <sub>IN</sub>	Input Voltage Range		0.7		3.6	V
	Minimum Startup Voltage	$I_{LOAD} = 1 \text{mA}, T_{AMB} = +25 ^{\circ}\text{C}$		0.7	0.8	V
		Regulation	ı		ı	
V <sub>OUT</sub>	Output Voltage Range		1.8		3.3	V
	O to tWilliam Talesco	I <sub>LOAD</sub> = 10 mA, T <sub>AMB</sub> = +25°C	-2		+2	%
	Output Voltage Tolerance	I <sub>LOAD</sub> = 10mA	-3		+3	%
	V <sub>OUT</sub> Lockout Threshold <sup>(1)</sup>	Rising Edge	1.55	1.65	1.75	V
		Operating Current				
la	Quiescent Current V <sub>IN</sub>	$V_{OUT} = 1.02xV_{OUTNOM'}$ $REF = 0.99xV_{OUTNOM'}$ $T_{AMB} = +25^{\circ}C$			100	nA
IQ	Quiescent Current V <sub>OUT</sub>	$V_{OUT} = 1.02 \text{xV}_{ON}$ , REF = 0.99xV <sub>ON</sub> , No load, $T_{AMB} = +25$ °C	0.8	1	1.2	μΑ
I <sub>SHDN</sub>	Shutdown Current	T <sub>AMB</sub> = +25°C			100	nA

ams Datasheet Page 5
[v1-11] 2015-Jan-28 Document Feedback



Symbol	Parameter	Conditions	Min	Тур	Max	Units				
	Switches									
R <sub>ON</sub>	NMOS	V <sub>OUT</sub> = 3V		0.35		Ω				
HON	PMOS	001 – 30		0.5		Ω				
	NMOS maximum On-time		3.6	4.2	4.8	μs				
I <sub>PEAK</sub>	Peak Current Limit		320	400	480	mA				
	Zero Crossing Current		5	20	35	mA				
		Enable, Reference		•						
VENH	EN Input Voltage High		0.7			V				
VENL	EN Input Voltage Low				0.1	V				
I <sub>EN</sub>	EN Input Bias Current	EN = 3.6V, T <sub>AMB</sub> = +25°C			100	nA				
I <sub>REF</sub>	REF Input Bias Current	$REF = 0.99xV_{OUTNOM'}$ $T_{AMB} = +25^{\circ}C$			100	nA				
	1	Low Battery & Power-OK		l	l					
V <sub>LBI</sub>	LBI Threshold	Falling Edge	0.57	0.6	0.63	V				
	LBI Hysteresis			25		mV				
I <sub>LBI</sub>	LBI Leakage Current	LBI = 3.6V, T <sub>AMB</sub> = +25°C			100	nA				
$V_{LBO}$	LBO Voltage Low <sup>(2)</sup>	ILBO = 1mA		20	100	mV				
I <sub>LBO</sub>	LBO Leakage Current	LBO = 3.6V, T <sub>AMB</sub> = +25°C			100	nA				
	Power-OK Threshold	LBI = 0V, Falling Edge	90	92.5	95	%				
		Thermal Protection								
	Thermal Shutdown	10°C Hysteresis		150		°C				

#### Note(s) and/or Footnote(s):

- 1. The regulator is in startup mode until this voltage is reached. Caution: Do not apply full load current until the device output > 1.75V.
- 2. LBO goes low in startup mode as well as during normal operation if:
  - The voltage at the LBI pin is below LBI threshold.
  - The voltage at the LBI pin is below 0.1V and  $\rm V_{OUT}$  is below 92.5% of its nominal value.

Page 6ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



# Typical Operating Characteristics

 $T_{AMB} = +25$ °C, unless otherwise specified.

Figure 7: Efficiency vs. Output Current; V<sub>OUT</sub> = 1.8V

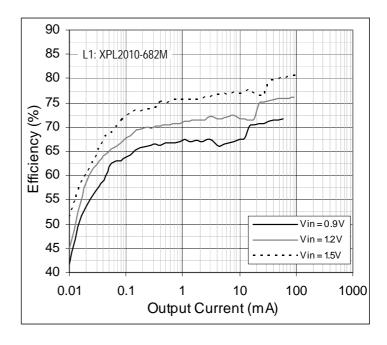
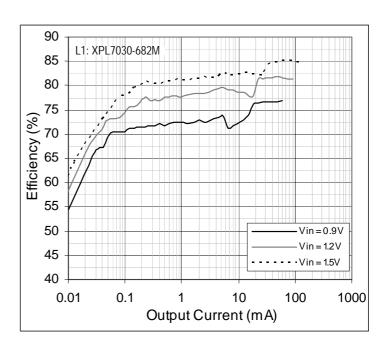


Figure 8: Efficiency vs. Output Current; V<sub>OUT</sub> = 1.8V



ams Datasheet Page 7
[v1-11] 2015-Jan-28
Document Feedback



Figure 9: Efficiency vs. Output Current; V<sub>OUT</sub> = 3.0V

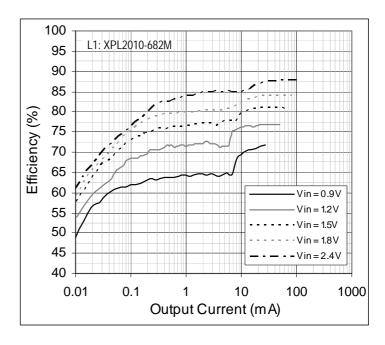
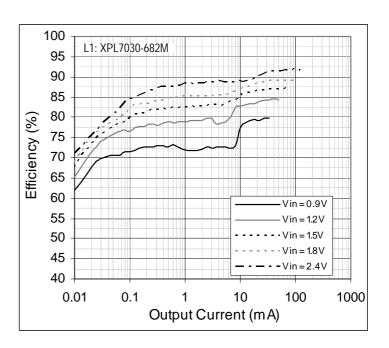


Figure 10: Efficiency vs. Output Current; V<sub>OUT</sub> = 3.0V



Page 8ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



Figure 11: Efficiency vs. Input Voltage; V<sub>OUT</sub> = 1.8V

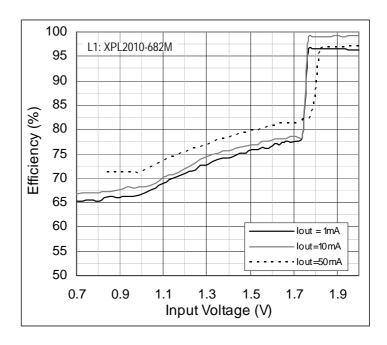
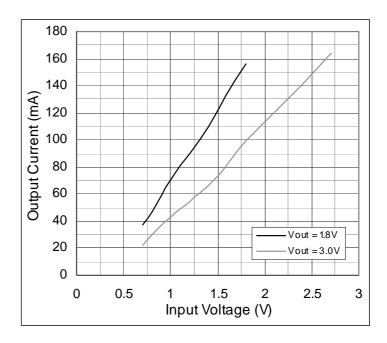


Figure 12:
Maximum Output Current vs. Input Voltage



ams Datasheet Page 9
[v1-11] 2015-Jan-28 Document Feedback



Figure 13: Start-up Voltage vs. Output Current

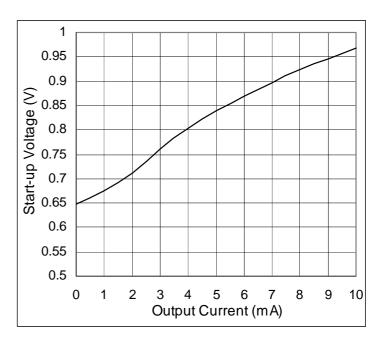
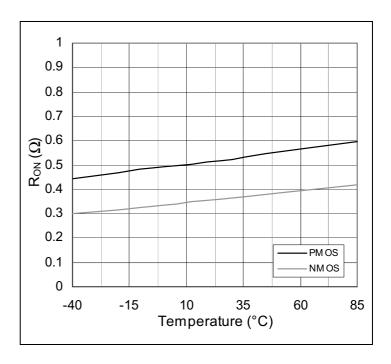


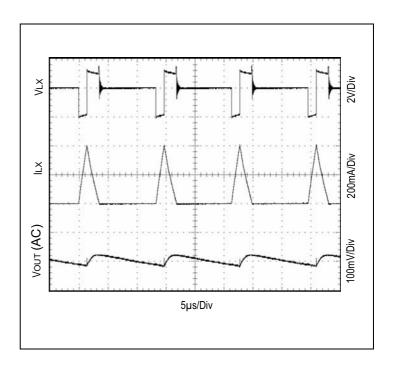
Figure 14: RON vs. Temperature



Page 10ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



Figure 15: Output Voltage Ripple;  $V_{IN}$  = 2V,  $V_{OUT}$  = 3V,  $R_{load}$  = 100  $\Omega$ 



ams Datasheet Page 11
[v1-11] 2015-Jan-28
Document Feedback



#### **Detailed Description**

#### **Hysteretic Boost Converter**

Hysteretic boost converters are so called because comparators are the active elements used to determine ON-OFF timing via current and voltage measurements. There is no continuously operating fixed oscillator, providing an independent timing reference. As a result, a hysteretic or comparator based converter has a very low quiescent current. In addition, because there is no fixed timing reference, the operating frequency is determined by external component (inductor and capacitors) and also the loading on the output.

Ripple at the output is an essential operating component. A power cycle is initiated when the output regulated voltage drops below the nominal value of  $V_{OUT}$  (0.99 x  $V_{OUT}$ ).

Inductor current is monitored by the control loop, ensuring that operation is always dis-continuous.

The application circuit shown in Figure 2 will support many requirements. However, further optimization may be useful, and the following is offered as a guide to changing the passive components to more closely match the end requirement.

#### **Input Loop Timing**

The input loop consists of the source DC supply, the input capacitor, the main inductor, and the N-channel power switch. The ON timing of the N-channel switch is determined by a peak current measurement or a maximum ON time. In the AS1310, peak current is 400mA (typ) and maximum ON time is 4.2µs (typ). Peak current measurement ensures that the ON time varies as the input voltage varies. This imparts line regulation to the converter.

The fixed ON-time measurement is something of a safety feature to ensure that the power switch is never permanently ON. The fixed on-time is independent of input voltage changes. As a result, no line regulation exists.

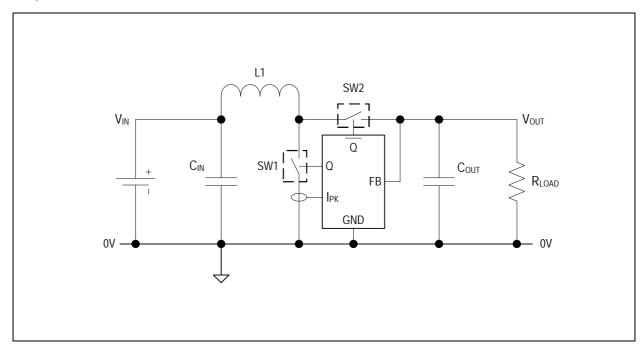
Page 12

Document Feedback

[v1-11] 2015-Jan-28



Figure 16: **Simplified Boost DCDC Architecture** 



ON time of the power switch (Faraday's Law) is given by:

$$(\text{EQ1}) \hspace{0.5cm} T_{ON} = \frac{LI_{PK}}{V_{IN} - (I_{PK}R_{SW1} + I_{PK}R_{L1})} \text{ sec [volts, amps, ohms, Henry]}$$

Applying Min and Max values and neglecting the resistive voltage drop across L1 and SW1;

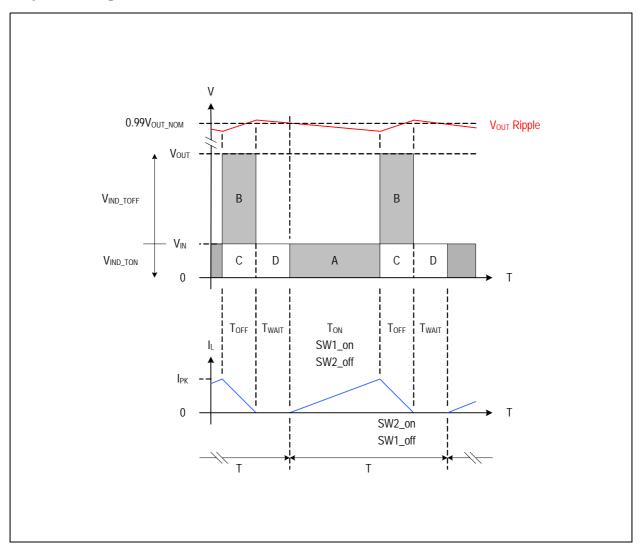
(EQ2) 
$$T_{ON\_MIN} = \frac{L_{MIN}I_{PK\_MIN}}{V_{IN\_MAX}}$$

(EQ3) 
$$T_{ON\_MAX} = \frac{L_{MAX}I_{PK\_MAX}}{V_{IN\_MIN}}$$

ams Datasheet Page 13 **Document Feedback** 



Figure 17: Simplified Voltage and Current Waveforms



Another important relationship is the "volt-seconds" law. Expressed as following:

(EQ4) 
$$V_{ON}T_{ON} = V_{OFF}T_{OFF}$$

Voltages are those measured across the inductor during each time segment. Figure 17 shows this graphically with the shaded segments marked "A & B". Re-arranging EQ 4:

$$\label{eq:continuity} \text{(EQ5)} \quad \frac{T_{ON}}{T_{OFF}} = \frac{V_{OUT} - V_{IN}}{V_{IN}}$$

The time segment called  $T_{WAIT}$  in Figure 17 is a measure of the "hold-up" time of the output capacitor. While the output voltage is above the threshold (0.99xV<sub>OUT</sub>), the output is assumed to be in regulation and no further switching occurs.

Page 14

Document Feedback

[v1-11] 2015-Jan-28



#### **Inductor Choice Example**

For the AS1310  $V_{IN\_MIN}$  = 0.9V,  $V_{OUT\_MAX}$  = 3.3V, EQ 5 gives  $T_{ON}$ =2.66 $T_{OFF}$ .

Let the maximum operating on-time =  $1\mu$ s.

Note that this is shorter than the minimum limit ON-time of 3.6 $\mu$ s. Therefore from EQ 5,  $T_{OFF}$  = 0.376 $\mu$ s. Using EQ 3,  $L_{MAX}$  is obtained:

 $L_{MAX} = 1.875 \mu H$ . The nearest preferred value is 2.2  $\mu H$ .

This value provides the maximum energy storage for the chosen fixed ON-time limit at the minimum  $V_{\rm IN}$ .

Energy stored during the ON time is given by:

(EQ6) 
$$E = 0.5L(I_{PK})^2$$
 Joules (Region A in Figure 17)

If the overall time period  $(T_{ON} + T_{OFF})$  is T, the power taken from the input is:

(EQ7) 
$$P_{IN} = \frac{0.5L(I_{PK})^2}{T}$$
 Watts

Assume output power is 0.8  $P_{\text{IN}}$  to establish an initial value of operating period T.

 $T_{WAIT}$  is determined by the time taken for the output voltage to fall to 0.99xV<sub>OUT</sub>. The longer the wait time, the lower will be the supply current of the converter. Longer wait times require increased output capacitance. Choose  $T_{WAIT} = 10\%$  T as a minimum starting point for maximum energy transfer. For very low power load applications, choose  $T_{WAIT} \ge 50\%$  T.

#### **Output Loop Timing**

The output loop consists of the main inductor, P-channel synchronous switch (or diode if fitted), output capacitor and load. When the input loop is interrupted, the voltage on the LX pin rises (Lenz's Law). At the same time a comparator enables the synchronous switch, and energy stored in the inductor is transferred to the output capacitor and load. Inductor peak current supports the load and replenishes the charge lost from the output capacitor. The magnitude of the current from the inductor is monitored, and as it approaches zero, the synchronous switch is turned ON. No switching action continues until the output voltage falls below the output reference point  $(0.99 \times V_{OUT})$ .

Output power is composed of the DC component (Region C in Figure 17):

(EQ8) 
$$P_{REGION\_C} = V_{IN} \frac{I_{PK}}{2} \frac{T_{OFF}}{T}$$

Output power is also composed of the inductor component (Region B in Figure 17), neglecting efficiency loss:

ams Datasheet Page 15
[v1-11] 2015-Jan-28 Document Feedback



(EQ9) 
$$P_{REGION\_B} = \frac{0.5L(I_{PK})^2}{T}$$

Total power delivered to the load is the sum of EQ 8 and EQ 9:

$$\label{eq:potal_pk} \text{(EQ10)} \quad P_{TOTAL} \, = \, V_{IN} \frac{I_{PK}}{2} \frac{T_{OFF}}{T} + \frac{0.5 L {(I_{PK})}^2}{T}$$

From EQ 3 (using nominal values) peak current is given by:

(EQ11) 
$$I_{PK} = \frac{T_{ON}V_{IN}}{L}$$

Substituting EQ 11 into EQ 10 and re-arranging:

(EQ12) 
$$P_{TOTAL} = \frac{V_{IN}^2 T_{ON}}{2TL} (0.9T)$$

0.9T incorporates a wait time T<sub>WAIT</sub> = 10% T

Output power in terms of regulated output voltage and load resistance is:

(EQ13) 
$$P_{OUT} = \frac{V_{OUT}^2}{R_{LOAD}}$$

Combining EQ 12 and EQ 13:

(EQ14) 
$$\frac{V_{OUT}^2}{R_{LOAD}} = \frac{V_{IN}^2 T_{ON}}{2TL} (0.9T) \eta$$

Symbol  $\eta$  reflects total energy loss between input and output and is approximately 0.8 for these calculations. Use EQ 14 to plot duty cycle ( $T_{ON}/T$ ) changes for various output loadings and changes to  $V_{IN}$ .

#### **Input Capacitor Selection**

The input capacitor supports the triangular current during the ON-time of the power switch, and maintains a broadly constant input voltage during this time. The capacitance value is obtained from choosing a ripple voltage during the ON-time of the power switch. Additionally, ripple voltage is generated by the equivalent series resistance (ESR) of the capacitor. For worst case, use maximum peak current values from the datasheet.

$$(\text{EQ15}) \quad C_{IN} = \frac{I_{PEAK}T_{ON}}{V_{RIPPLE}}$$

Using  $T_{ON} = 1 \mu s$ , and  $I_{PEAK} = 480 mA$ , and  $V_{RIPPLE} = 50 mV$ , EQ 15 yields:

$$C_{IN} = 9.6 \mu F$$

Nearest preferred would be 10µF.

$$(EQ16) \quad V_{PK\_RIPPLE\_ESR} = I_{PK}R_{ESR}$$

Page 16

Document Feedback

[v1-11] 2015-Jan-28



Typically, the ripple due to ESR is not dominant. ESR for the recommended capacitors (Murata GMR), ESR =  $5m\Omega$  to  $10m\Omega$ . For the AS1310, maximum peak current is 480mA. Ripple due to ESR is 2.4mV to 4.8mV.

Ripple at the input propagates through the common supply connections, and if too high in value can cause problems elsewhere in the system. The input capacitance is an important component to get right.

#### **Output Capacitor Selection**

The output capacitor supports the triangular current during the OFF-time of the power switch (inductor discharge period), and also the load current during the wait time (Region D in Figure 17) and ON-time (Region A in Figure 17) of the power switch.

(EQ17) 
$$C_{OUT} = \frac{I_{LOAD}(T_{ON} + T_{WAIT})}{(1 - 0.99)V_{OUT NOM}}$$

**Note(s):** There is also a ripple component due to the equivalent series resistance (ESR) of the capacitor.

#### **Summary**

#### **User Application Defines:**

V<sub>INmin</sub>, V<sub>INmax</sub>, V<sub>OUTmin</sub>, V<sub>OUTmax</sub>, I<sub>LOADmin</sub>, I<sub>LOADmax</sub>

#### **Inductor Selection:**

Select Max on-time =  $0.5\mu s$  to  $3\mu s$  for AS1310. Use EQ 3 to calculate inductor value.

Use EQ 5 to determine OFF-time.

Use EQ 6 to check that power delivery matches load requirements assume 70% conversion efficiency.

Use EQ 13 to find overall timing period value of T at min  $V_{IN}$  and max  $V_{OUT}$  for maximum load conditions.

#### **Input Capacitor Selection:**

Choose a ripple value and use EQ 14 to find the value.

#### **Output Capacitor Selection:**

Determine  $T_{\text{WAIT}}$  via EQ 6 or EQ 13, and use EQ 16 to find the value.

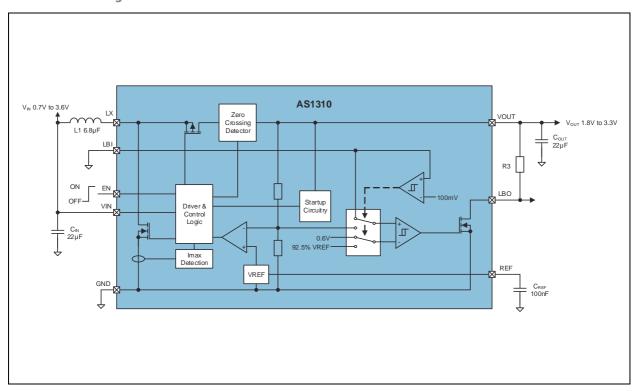
ams Datasheet Page 17
[v1-11] 2015-Jan-28 Document Feedback



#### **Application Information**

The AS1310 is available with fixed output voltages from 1.8V to 3.3V in 50mV steps.

Figure 18: AS1310 Block Diagram



#### **AS1310 Features**

**Shutdown**. The part is in shutdown mode while the voltage at pin EN is below 0.1V and is active when the voltage is higher than 0.7V.

**Note(s):** EN can be driven above  $V_{\text{IN}}$  or  $V_{\text{OUT}}$ , as long as it is limited to less than 3.6V.

**Output Disconnect and Inrush Limiting**. During shutdown  $V_{OUT}$  is going to 0V and no current from the input source is running through the device. This is true as long as the input voltage is higher than the output voltage.

**Feedthrough Mode.** If the input voltage is higher than the output voltage the supply voltage is connected to the load through the device. To guarantee a proper function of the AS1310 it is not allowed that the supply exceeds the maximum allowed input voltage (3.6V).

In this feedthrough mode the quiescent current is  $35\mu A$  (typ.). The device goes back into step-up mode when the oputput voltage is 4% (typ.) below  $V_{OUTNOM}$ .

Page 18
Document Feedback

[v1-11] 2015-Jan-28



#### Power-OK and Low-Battery-Detect Functionality

LBO goes low in startup mode as well as during normal operation if:

- The voltage at the LBI pin is below LBI threshold (0.6V). This can be used to monitor the battery voltage.
- $\bullet$  LBI pin is connected to GND and  $V_{OUT}$  is below 92.5% of its nominal value. LBO works as a power-OK signal in this case.

The LBI pin can be connected to a resistive-divider to monitor a particular definable voltage and compare it with a 0.6V internal reference. If LBI is connected to GND an internal resistive-divider is activated and connected to the output. Therefore, the Power-OK functionality can be realized with no additional external components.

The Power-OK feature is not active during shutdown and provides a power-ON-reset function that can operate down to  $V_{IN}=0.7V$ . A capacitor to GND may be added to generate a power-ON-reset delay. To obtain a logic-level output, connect a pull-up resistor R3 from pin LBO to pin  $V_{OUT}$ . Larger values for this resistor will help to minimize current consumption; a  $100k\Omega$  resistor is perfect for most applications (see Figure 20).

For the circuit shown in the left of Figure 19, the input bias current into LBI is very low, permitting large-value resistor-divider networks while maintaining accuracy. Place the resistor-divider network as close to the device as possible. Use a defined resistor for R<sub>2</sub> and then calculate R<sub>1</sub> as:

$$\text{(EQ18)} \quad R_1 \, = \, R_2 \cdot \left( \frac{V_{\mathrm{IN}}}{V_{\mathrm{LBI}}} - 1 \right)$$

Where: V<sub>LBI</sub> is 0.6V ±30mV

ams Datasheet Page 19
[v1-11] 2015-Jan-28 Document Feedback



Figure 19: Typical Application with Adjustable Battery Monitoring

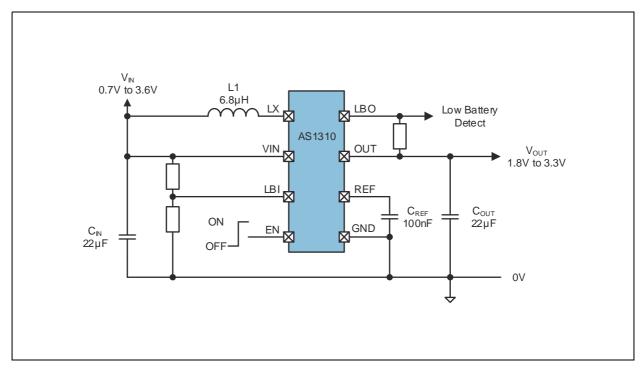
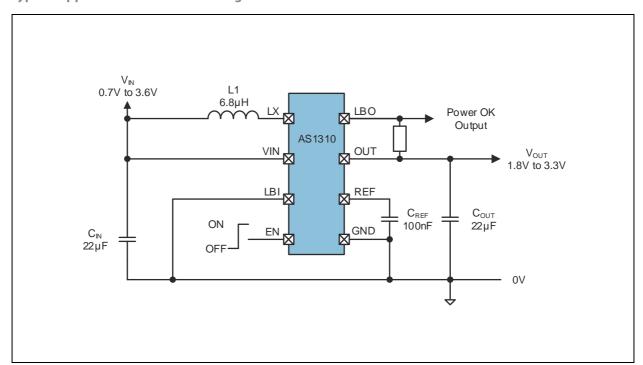


Figure 20:
Typical Application with LBO working as Power-OK



Page 20ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



#### Thermal Shutdown

To prevent the AS1310 from short-term misuse and overload conditions the chip includes a thermal overload protection. To block the normal operation mode all switches will be turned OFF. The device is in thermal shutdown when the junction temperature exceeds 150°C. To resume the normal operation the temperature has to drop below 140°C.

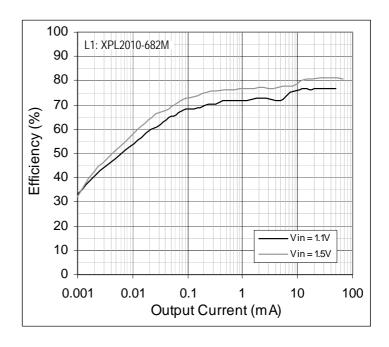
A good thermal path has to be provided to dissipate the heat generated within the package. Otherwise it's not possible to operate the AS1310 at its usable maximal power. To dissipate as much heat as possible from the package into a copper plane with as much area as possible, it's recommended to use multiple vias in the printed circuit board. It's also recommended to solder the Exposed Pad (pin 9) to the GND plane.

**Note(s):** Continuing operation in thermal overload conditions may damage the device and is considered bad practice.

#### **Always ON Operation**

In battery powered applications with long standby times as blood glucose meters, remote controls, soap dispensers, etc., a careful battery management is required. Normally a complex power management control makes sure that the DCDC is only switched ON, when it is really needed. With AS1310 this complex control can be saved completely, since the AS1310 is perfectly suited to support always-ON operations of the application. The efficiency at standby currents of e.g.  $2\mu As$  is around 45% (see Figure 21).

Figure 21: Efficiency vs. Output Current for Always ON Operation;  $V_{OUT}$ =3.3V



ams Datasheet Page 21
[v1-11] 2015-Jan-28 Document Feedback



#### **Component Selection**

Only four components are required to complete the design of the step-up converter. The low peak currents of the AS1310 allow the use of low value, low profile inductors and tiny external ceramic capacitors.

#### **Inductor Selection**

For best efficiency, choose an inductor with high frequency core material, such as ferrite, to reduce core losses. The inductor should have low DCR (DC resistance) to reduce the  $I^2R$  losses, and must be able to handle the peak inductor current without saturating. A 6.8µH inductor with a >500mA current rating and <500m $\Omega$  DCR is recommended.

Figure 22: Recommended Inductors

Part Number	L	DCR	Current Rating	Dimensions (L/W/T)	Manufacturer
XPL2010-682M	6.8µH	421mΩ	0.62A	2.0x1.9x1.0 mm	
EPL2014-682M	6.8µH	287mΩ	0.59A	2.0x2.0x1.4 mm	
LPS3015-682M	6.8µH	300m $Ω$	0.86A	3.0x3.0x1.5 mm	Coilcraft
LPS3314-682M	6.8µH	240mΩ	0.9A	3.3x3.3x1.3 mm	www.coilcraft.com
LPS4018-682M	6.8µH	150mΩ	1.3A	3.9x3.9x1.7 mm	
XPL7030-682M	6.8µH	59mΩ	9.4A	7.0x7.0x3.0 mm	
LQH32CN6R8M53L	6.8µH	250m $\Omega$	0.54A	3.2x2.5x1.55 mm	
LQH3NPN6R8NJ0L	6.8µH	210mΩ	0.7A	3.0x3.0x1.1 mm	Murata www.murata.com
LQH44PN6R8MJ0L	6.8µH	143m $\Omega$	0.72A	4.0x4.0x1.1 mm	

Page 22

Document Feedback

[v1-11] 2015-Jan-28



#### **Capacitor Selection**

The convertor requires three capacitors. Ceramic X5R or X7R types will minimize ESL and ESR while maintaining capacitance at rated voltage over temperature. The  $V_{\text{IN}}$  capacitor should be  $22\mu\text{F}$ . The  $V_{\text{OUT}}$  capacitor should be between  $22\mu\text{F}$  and  $47\mu\text{F}$ . A larger output capacitor should be used if lower peak to peak output voltage ripple is desired. A larger output capacitor will also improve load regulation on  $V_{\text{OUT}}$ . See Figure 23 for a list of capacitors for input and output capacitor selection.

Figure 23: Recommended Input and Output Capacitors

Part Number	С	TC Code	Rated Voltage	Dimensions (L/W/T)	Manufacturer
GRM21BR60J226ME99	22μF	X5R	6.3V	0805, T=1.25mm	
GRM31CR61C226KE15	22μF	X5R	16V	1206, T=1.6mm	Murata www.murata.com
GRM31CR60J475KA01	47μF	X5R	6.3V	1206, T=1.6mm	

On the pin REF a 10nF capacitor with an Insulation resistance  $>1G\Omega$  is recommended.

Figure 24: Recommended Capacitors for REF

Part Number	С	TC Code	Insulation Resistance	Rated Voltage	Dimensions (L/W/T)	Manufacturer
GRM188R71C104KA01	100nF	X7R	>5GΩ	16V	0603, T=0.8mm	Murata
GRM31CR61C226KE15	100nF	X7R	>5 <b>G</b> Ω	50V	0805, T=1.25mm	www.murata.com

#### **Layout Considerations**

Relatively high peak currents of 480mA (max) circulate during normal operation of the AS1310. Long printed circuit tracks can generate additional ripple and noise that mask correct operation and prove difficult to "de-bug" during production testing. Referring to Figure 2, the input loop formed by C1,  $V_{IN}$  and GND pins should be minimized. Similarly, the output loop formed by C2,  $V_{OUT}$  and GND should also be minimized. Ideally both loops should connect to GND in a "star" fashion. Finally, it is important to return  $C_{REF}$  to the GND pin directly.

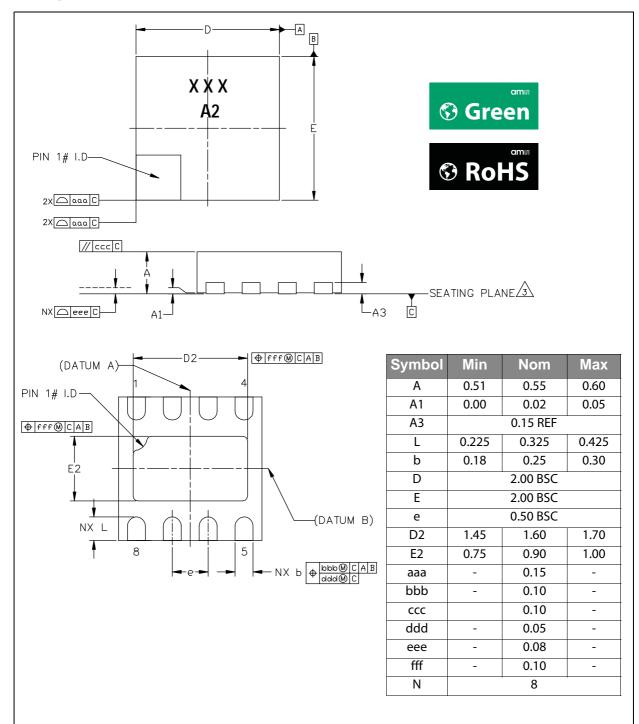
ams Datasheet Page 23
[v1-11] 2015-Jan-28 Document Feedback



#### Package Drawings & Markings The device is

The device is available in a TDFN (2x2) 8-pin package.

Figure 25: Drawings and Dimensions



#### Note(s) and/or Footnote(s):

- 1. Dimensioning & tolerancing conform to ASME Y14.5M-1994.
- $2. \ All \ dimensions \ are \ in \ millimeters. \ Angles \ are \ in \ degrees.$
- 3. Coplanarity applies to the exposed heat slug as well as the terminal.
- 4. Radius on terminal is optional.
- 5. N is the total number of terminals.

Page 24

Document Feedback

[v1-11] 2015-Jan-28



Ordering & Contact Information The device is available as the standard products shown in Figure 26.

Figure 26: **Ordering Information** 

Ordering Code	Marking	Output	Description	Delivery Form	Package
AS1310-BTDT-18	A2	1.8V		Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-20	A8	2.0V		Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-25	A9	2.5V	Ultra Low Quiescent	Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-27	A7	2.7V	Current, Hysteretic DC-DC	Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-30	A6	3.0V	Step-Up Converter	Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-33 <sup>(1)</sup>	tbd	3.3V		Tape and Reel	TDFN (2x2) 8-pin
AS1310-BTDT-xx <sup>(2)</sup>	tbd	tbd		Tape and Reel	TDFN (2x2) 8-pin

#### Note(s) and/or Footnote(s):

- 1. On request
- 2. Non-standard devices are available between 1.8V and 3.3V in 50mV steps.

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#### Headquarters

ams AG Tobelbaderstrasse 30 8141 Unterpremstaetten Austria, Europe

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ams Datasheet Page 25 Document Feedback



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Page 26

Document Feedback

[v1-11] 2015-Jan-28



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ams Datasheet Page 27 **Document Feedback** 



## **Document Status**

Document Status	Product Status	Definition
Product Preview Pre-Development		Information in this datasheet is based on product ideas in the planning phase of development. All specifications are design goals without any warranty and are subject to change without notice
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Page 28ams DatasheetDocument Feedback[v1-11] 2015-Jan-28



### **Revision Information**

Changes from 1-10 (2014-Nov-11) to current revision 1-11 (2015-Jan-28)	Page
Updated Figure 18	18
Updated Figures 19 & 20	20

#### Note(s) and/or Footnote(s):

- 1. Page and figure numbers for the previous version may differ from page and figure numbers in the current revision.
- 2. Correction of typographical errors is not explicitly mentioned.

ams Datasheet Page 29 Document Feedback



#### **Content Guide**

- 1 General Description
- 1 Key Benefits & Features
- 2 Applications
- 3 Pin Assignment
- 4 Absolute Maximum Ratings
- 5 Electrical Characteristics
- 7 Typical Operating Characteristics

#### 12 Detailed Description

- 12 Hysteretic Boost Converter
- 12 Input Loop Timing
- 15 Inductor Choice Example
- 15 Output Loop Timing
- 16 Input Capacitor Selection
- 17 Output Capacitor Selection
- 17 Summary

#### 18 Application Information

- 18 AS1310 Features
- 19 Power-OK and Low-Battery-Detect Functionality
- 21 Thermal Shutdown
- 21 Always ON Operation
- 22 Component Selection
- 22 Inductor Selection
- 23 Capacitor Selection
- 23 Layout Considerations
- 24 Package Drawings & Markings
- 25 Ordering & Contact Information
- 26 RoHS Compliant & ams Green Statement
- 27 Copyrights & Disclaimer
- 28 Document Status
- 29 Revision Information

Page 30

Document Feedback

[v1-11] 2015-Jan-28