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NO RECOMMENDED REPLACEMENT**  
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## Antilog Amplifier

### Features

- Full Scale Accuracy ..... 0.5%
- Temperature Compensated Operation .... 0°C to 70°C
- Scale Factor, Adjustable ..... 1V/Decade
- Dynamic Voltage Range ..... 60dB
- Dual JFET Input Op Amps

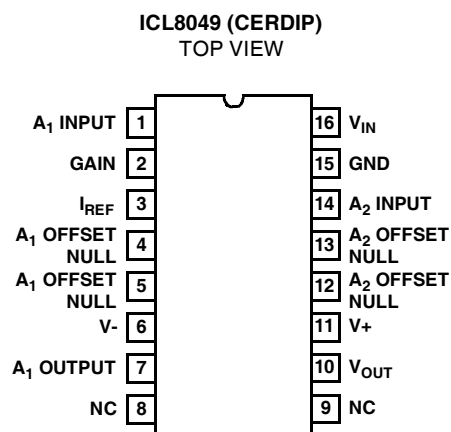
### Description

The ICL8049 is a monolithic antilogarithmic amplifier that is fully temperature compensated and is nominally designed to provide 1 decade of output voltage for each 1V change of input voltage. For increased flexibility, the scale factor, reference current and offset voltage are externally adjustable.

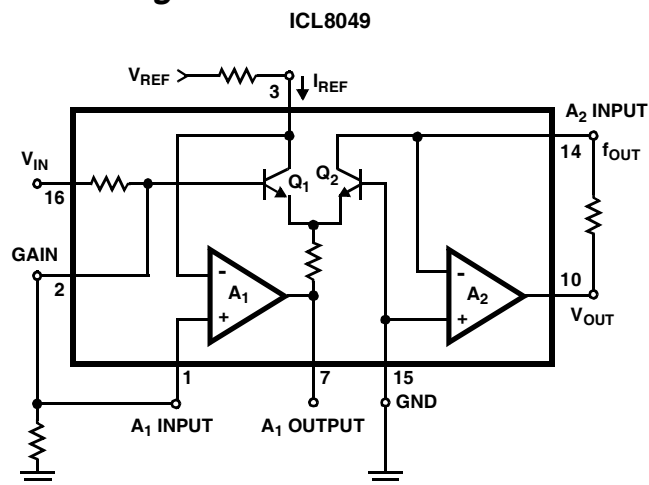
### Part Number Information

PART NUMBER	ERROR (25°C)	TEMPERATURE RANGE (°C)	PACKAGE
ICL8049BCJE	10mV	0 to 70	16 Ld CERDIP
ICL8049CCJE	25mV	0 to 70	16 Ld CERDIP

### Pinout



### Functional Diagram



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# ICL8049

## Absolute Maximum Ratings

Supply Voltage .....  $\pm 18V$   
 $V_{IN}$  (Input Current) .....  $\pm 15V$   
 $I_{REF}$  (Reference Current) .....  $2mA$   
Voltage Between Offset Null and  $V+$  .....  $\pm 0.5V$   
Output Short Circuit Duration ..... Indefinite  
Power Dissipation .....  $750mW$   
Lead Temperature (Soldering 10 Sec.) .....  $300^{\circ}C$

## Operating Conditions

Operating Temperature Range .....  $0^{\circ}C$  to  $70^{\circ}C$   
Storage Temperature Range .....  $-65^{\circ}C$  to  $150^{\circ}C$

*CAUTION: Stresses above those listed in "Absolute Maximum Ratings" may cause permanent damage to the device. This is a stress only rating and operation of the device at these or any other conditions above those indicated in the operational sections of this specification is not implied.*

**Electrical Specifications**  $V_S = \pm 15V$ ,  $T_A = 25^{\circ}C$ ,  $I_{REF} = 1mA$ , Scale Factor Adjusted for 1 Decade (Out) per Volt (In), Unless Otherwise Specified

PARAMETERS	TEST CONDITIONS	ICL4049BC			ICL8049CC			UNITS
		MIN	TYP	MAX	MIN	TYP	MAX	
Dynamic Range ( $V_{OUT}$ )	$V_{OUT} = 10mV$ to $10V$	60	-	-	60	-	-	dB
Error, Absolute Value	$0V \leq V_{IN} \leq 2V$	-	3	15	-	5	25	mV
	$T_A = 0^{\circ}C$ to $70^{\circ}C$ , $0V \leq V_{IN} \leq 3V$	-	20	75	-	30	150	mV
Temperature Coefficient, Referred to $V_{IN}$	$V_{IN} = 3V$	-	0.38	-	-	0.55	-	$mV/^{\circ}C$
Power Supply Rejection Ratio	Referred to Input, for $V_{IN} = 0V$	-	2.0	-	-	2.0	-	$\mu V/V$
Offset Voltage ( $A_1$ and $A_2$ )	Before Nulling	-	15	25	-	15	50	mV
Wideband Noise	Referred to Input, for $V_{IN} = 0V$	-	26	-	-	26	-	$\mu V_{RMS}$
Output Voltage Swing	$R_L = 10k\Omega$	$\pm 12$	$\pm 14$	-	$\pm 12$	$\pm 14$	-	V
	$R_L = 2k\Omega$	$\pm 10$	$\pm 13$	-	$\pm 10$	$\pm 13$	-	V
Power Consumption		-	150	200	-	150	200	mW
Supply Current		-	5	6.7	-	5	6.7	mA

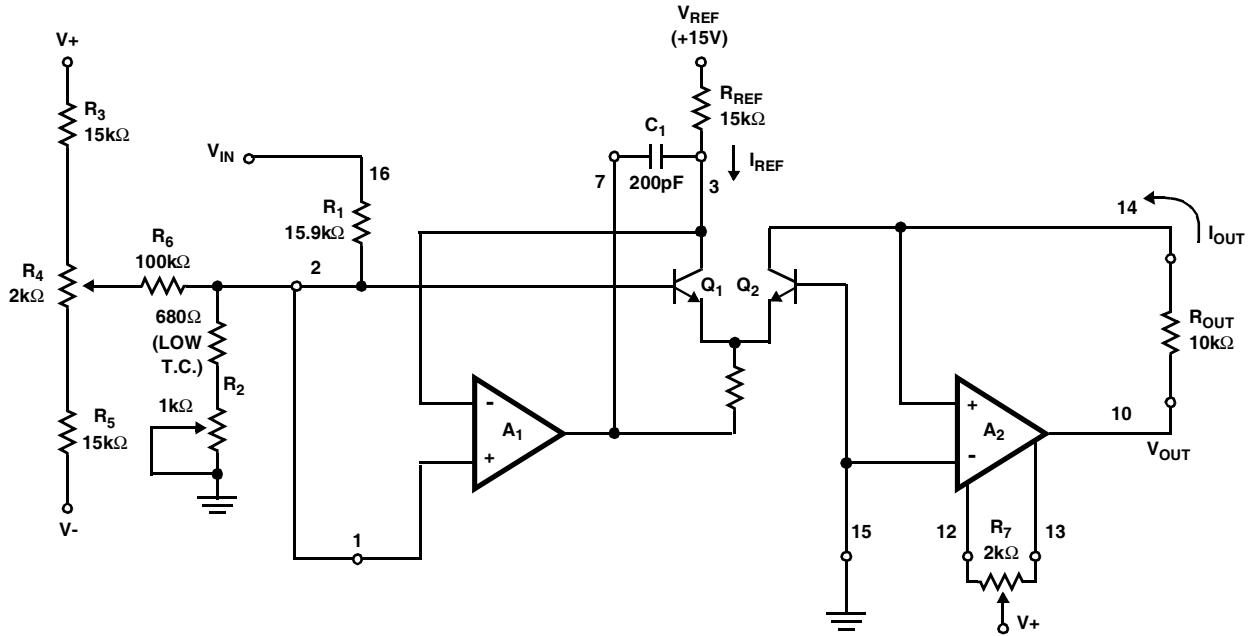


FIGURE 1. ICL8049 OFFSET AND SCALE FACTOR ADJUSTMENT

### ICL8049 Detailed Description

The ICL8049 relies on the same logarithmic properties of the transistor as the ICL8048. The input voltage forces a specific  $\Delta V_{BE}$  between  $Q_1$  and  $Q_2$  (Figure 1). This  $V_{BE}$  difference is converted into a difference of collector currents by the transistor pair. The equation governing the behavior of the transistor pair is derived from (2) on the previous page and is as follows:

$$\frac{I_{C1}}{I_{C2}} = \exp\left[\frac{q\Delta V_{BE}}{kT}\right] \quad (1)$$

When numerical values for  $q/kT$  are put into this equation, it is found that a  $\Delta V_{BE}$  of 59mV (at +25°C) is required to change the collector current ratio by a factor of ten. But for ease of application, it is desirable that a 1V change at the input generate a tenfold change at the output. The required input attenuation is achieved by the network comprising  $R_1$  and  $R_2$ . In order that scale factors other than one decade per volt may be selected,  $R_2$  is external to the chip. It should have a value of 1kΩ, adjustable  $\pm 20\%$ , for one decade per volt.  $R_1$  is a thin film resistor deposited on the monolithic chip; its temperature characteristics are chosen to compensate the temperature dependence of Equation 1, as explained on the previous page.

The overall transfer function is as follows:

$$\frac{I_{OUT}}{I_{REF}} = \exp\left[\frac{-R_2}{(R_1 + R_2)} \times \frac{qV_{IN}}{kT}\right] \quad (2)$$

Substituting  $V_{OUT} = I_{OUT} \times R_{OUT}$  gives:

$$V_{OUT} = R_{OUT} I_{REF} \exp\left[\frac{-R_2}{(R_1 + R_2)} \times \frac{qV_{IN}}{kT}\right] \quad (3)$$

For voltage references Equation 3 becomes

$$V_{OUT} = V_{REF} \times \frac{R_{OUT}}{R_{REF}} \exp\left[\frac{-R_2}{(R_1 + R_2)} \times \frac{qV_{IN}}{kT}\right] \quad (4)$$

### ICL8049 Offset and Scale Factor Adjustment

As with the log amplifier, the antilog amplifier requires three adjustments. The first step is to null out the offset voltage of  $A_2$ . This is accomplished by reverse biasing the base-emitter of  $Q_2$ .  $A_2$  then operates as a unity gain buffer with a grounded input. The second step forces  $V_{IN} = 0$ ; the output is adjusted for  $V_{OUT} = 10V$ . This step essentially "anchors" one point on the transfer function. The third step applies a specific input and adjusts the output to the correct voltage. This sets the scale factor. Referring to Figure 1 the exact procedure for 1 decade/volt is as follows:

1. Connect the input (pin #16) to +15V. This reverse biases the base-emitter of  $Q_2$ . Adjust  $R_7$  for  $V_{OUT} = 0V$ . Disconnect the input from +15V.
2. Connect the input to Ground. Adjust  $R_4$  for  $V_{OUT} = 10V$ . Disconnect the input from Ground.
3. Connect the input to a precise 2V supply and adjust  $R_2$  for  $V_{OUT} = 100mV$ .

The procedure outlined above optimizes the performance over a 3 decade range at the output (i.e.,  $V_{OUT}$  from 10mV to 10V). For a more limited range of output voltages, for example 1V to 10V, it would be better to use a precise 1V supply and adjust for  $V_{OUT} = 1V$ . For other scale factors and/or starting points, different values for  $R_2$  and  $R_{REF}$  will be needed, but the same basic procedure applies.